

UNITED STATES OF AMERICA

TO ALL WHOM IT MAY CONCERN:

BE IT KNOWN THAT I, RAAFAT R. MANSOUR of 310
Amberwood Drive, Waterloo, Ontario Canada, N2T 2G2, Canadian Citizen, have
invented certain new and useful improvements in

MODIFIED CONDUCTOR LOADED CAVITY RESONATOR
WITH IMPROVED SPURIOUS PERFORMANCE, of which the following is a
specification:-

BACKGROUND OF THE INVENTION

FIELD OF INVENTION

5 The present invention is related to microwave bandpass filters and more particularly to the realization of compact size conductor-loaded cavity filters for use in space, wireless applications and other applications where size and spurious performance of the bandpass filters are critical.

10 DESCRIPTION OF THE PRIOR ART

Microwave filters are key components of any communication systems. Such a system, be it wireless or satellite, requires filters to separate the signals received into channels for amplification and processing. The phenomenal growth in telecommunication industry in
15 recent years has brought significant advances in filter technology as new communication systems emerged demanding equipment miniaturization while requiring more stringent filter characteristics. Over the past decade, the dielectric resonator technology has been the technology of choice for passive microwave filters for wireless and satellite applications.

20 Figure 1 illustrates the traditional dual-mode conductor-loaded cavity resonator. The resonator 1 is mounted in a planar configuration inside a rectangular cavity 2. Table 1 provides the resonant frequency of the first three resonant modes.

25 Table 1 Resonant frequency of prior art dual-mode conductor loaded cavity resonators
Metal puck: (0.222" x 2.4" dia),Rectangular cavity: (1.9" x 3.2" x 3.2")
Cylindrical cavity: 1.9" x 3.2" dia.

Mode	Resonant Frequency Rectangular Cavity	Resonant Frequency Cylindrical Cavity
Mode 1	1.889 GHz	1.940 GHz
Mode 2	2.506 GHz	2.733 GHz
Mode 3	3.434 GHz	3.322 GHz

30 SUMMARY OF THE INVENTION

It is an object of the present invention to provide a novel configuration etc. both single mode and dual mode dielectric resonator

filters have been employed for such applications. It is a further object of the present invention to provide a conductor-loaded cavity resonator filter that can be used in conventional and cryogenic applications. It is still another object of the present invention to provide a filter that is compact in size with a remarkable loss spurious performance compared to previous filters.

A microwave cavity has at least one wall. The cavity has a cut resonator located therein, the resonator being out of contact with the at least one wall.

10 A bandpass filter has at least one cavity. The at least one cavity has a cut resonator therein. The cavity has at least one wall and the resonator is out of contact with the at least one wall.

15 A method of improving the spurious performance of a bandpass filter, the method comprising a cut resonator in at least one cavity of the filter, the cavity having at least one wall and the resonator being located out of contact with the at least one wall.

BRIEF DESCRIPTION OF THE DRAWINGS

In the drawings:

Figure 1 is a perspective view of a prior art dual mode conductor-
20 loaded cavity resonator where the resonator is mounted inside a metallic enclosure;

Figure 2 is a perspective view of a half cut resonator contained within a cavity;

25 Figure 3 is a perspective view of a modified half cut resonator contained within a cavity;

Figure 4 is a top view of a shaped resonator;

Figure 5 is a top view of a two pole filter containing shaped resonators;

30 Figure 6 is a graph showing the measured isolation results of the filter described in Figure 5;

Figure 7 is a schematic top view of an 8-pole filter having

conductor-loaded resonators in two cavities and dielectric resonators in the remaining cavity;

Figure 8 is a schematic top view of an 8-pole filter having conductor-loaded resonators in three cavities and dielectric resonators in the remaining cavity;

Figure 9 is a schematic top view of a dual-mode filter having two conductor loaded resonators in each cavity.

DESCRIPTION OF A PREFERRED EMBODIMENT

The resonator of Figure 1 is a metallic resonator and the cavity 2 is a metallic enclosure. The electric field of the first mode resembles the TE₁₁ in cylindrical cavities. Thus, the use of a magnetic wall symmetry will not change the field distribution and consequently the resonant frequency.

In Figure 2, there is shown a half cut resonator 3 mounted in a cavity 4. It can be seen that the resonator 3 has a semicircular shape. The resonator 3 is mounted on a support (not shown) and is out of contact with walls of the cavity 4. The resonator 3 does not touch the walls of the cavity 4. The cavity 4 has almost half the volume of the cavity 2 shown in Figure 1. A dielectric support structure (not shown) is used in both Figures 1 and 2 to support the resonator.

With the use of the magnetic wall symmetry concept, a half-cut version of the conductor-loaded resonator with a modified shape can be realized as shown in Figure 3. The half-cut resonator would have a slightly higher resonant frequency with a size that is 50% of the original dual-mode cavity. The technique proposed in Wang et al "Dual mode conductor-loaded cavity filters" I. EEE Transactions on Microwave Theory and Techniques, V45, N. 8, 1997 can be applied for shaping dielectric resonators to conductor-loaded cavity resonators. In Figure 4, there is shown a top view of the modified half-cut resonator of Figure 3. The original half-cut resonator described in Figure 2 is selectively machined to enhance the separation between the resonant frequencies of

the dominant and the first higher-order mode. It can be seen that a substantially rectangular cutaway portion exists in a straight edge of the resonator 5 and a larger rectangular shaped cut away portion is located in the arcuate edge of the resonator 5. Both of the cut away portions are substantially centrally located.

Table 2 provides the resonant frequencies of the first three modes of the half-cut conductor-loaded resonator. Even though the TM mode has been shifted away, the spurious performance of the resonator has degraded.

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Table 2 The resonant frequencies of the first three modes of the half-cut conductor-loaded resonator

Mode	Resonant Frequency
Mode 1	2.119 GHz
Mode 2	2.234 GHz
Mode 3	3.824 GHz

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Table 3 gives the resonant frequencies of the first three modes of the modified half-cut resonator. A comparison between Tables 2 and 3 illustrates that the spurious performance of the modified half-cut resonator is superior to that of dual-mode resonators. It is interesting to note that shaping the resonator as shown in Figure 3 has shifted Mode 1 down in frequency while shifting Mode 2 up in frequency. This translates to a size reduction and a significant improvement in spurious performance.

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Table 3. The resonant frequencies of the first three modes of the modified half-cut conductor-loaded resonator

Mode	Resonate Frequency
Mode 1	1.559 GHz
Mode 2	2.980 GHz
Mode 3	3.535 GHz

It is well known that dielectric resonators filters suffer from limitations in spurious performance and power handling capability. By combining the dielectric resonators with the resonator disclosed in this invention both the spurious performance and power handling capability of dielectric resonator filters can be considerably improved.

Figure 4 shows a resonator 5 mounted inside an enclosure 6. The resonator 5 is a modified version of the resonator 3 shown in Figure 2 where a metal is machined out in specific areas to improve the spurious performance of the resonator. Figure 4 is an actual picture of the resonator 5 in the open cavity 6.

Figure 5 shows a picture of a two pole filter built using the resonator 5. The filter consists of two resonators coupled by an iris (not shown). Figure 6 shows the experimental isolation results of the filter shown in Figure 5. The results demonstrate the improvement in spurious performance. The spurious area is located at approximately twice the filter centre frequency.

Figure 7 shows an eight-pole filter where six dielectric resonators 6 are used in six cavities 7 in combination with two half-cut metallic resonators 5 in two cavities 7. The RF energy is coupled to the filter through input/output probes 8, 9 respectively. The metallic resonators could be placed horizontally as shown in Figure 7 or vertically. Even though the dielectric resonator filters have a limited spurious performance, the addition of the two metallic resonators considerably improves the overall spurious performance of the filter. In Figure 7, the metallic resonators are placed in the first and last cavities. However, metallic resonators can be placed in any of the cavities. .

Figure 8 shows an eight-pole filter where five dielectric resonators 6 are located in five cavities 7 in combination with three half-cut metallic resonators 5 located in three cavities 7. The RF energy is coupled to the filter through input/output probes 8, 9 respectively. The metallic resonators are placed in the first three cavities to improve the power handling capability of the dielectric resonator filter. It well known that, in high power applications,

high electric field will build up in the first three cavities. Such high field translates into heat, which in turn degrades the Q of the resonator, and affects the integrity of the support structure. The problem can be circumvented by replacing the dielectric resonators in these cavities with metallic resonators
5 disclosed in this invention. In both Figure 7 and Figure 8, there is one resonator in each cavity.

Figure 9 shows a four pole dual-mode filter consisting of two dual-mode resonators 10 in each cavity 7. Each dual-mode resonator is formed by combining two single-mode resonators 5. The end result is a compact dual-mode resonator with an improved spurious performance.
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A combination of dielectric resonators and conductor-loaded cavity resonators in the same filter improves the spurious performance of dielectric resonator filters over dielectric resonator filters that do not have any conductor-loaded cavity resonators. The use of conductor-loaded cavity
15 resonators in the same filter in combination with dielectric resonators extend the power handling capability of dielectric resonator filters.

Various materials are suitable for the resonators. For example, the resonator can be made of any metal or it can be made of superconductive material either by a thick film coating or bulk superconductor materials or
20 single crystal or by other means. Copper is an example of a suitable metal.